

PRACTICAL TESTS OF CURRENT FOLLOWER BASED ON DISCRETE COMMERCIALY AVAILABLE TRANSISTORS

Zdeněk Hruboš

Doctoral Degree Programme (1), FEEC BUT
E-mail: xhrubo00@stud.feec.vutbr.cz

Roman Šotner

Doctoral Degree Programme (2), FEEC BUT
E-mail: xsotne00@stud.feec.vutbr.cz

Supervised by: Jiří Petržela

E-mail: petrzelj@feec.vutbr.cz

ABSTRACT

Analyses and corresponding results of multi-output current follower (MO-CF) based on discrete commercially available transistors are presented in this paper. This element is very important for current-mode approaches and circuit design. Mentioned structure consists of minimum number of the transistors. There are discussed two two-output conceptions. First type produces positive polarities of output current and second type produces both polarities. The first one was experimentally tested. Related results in frequency domain, dynamical range and important small signal parameters are discussed. Simulation and measurements results are compared.

1. INTRODUCTION

The current followers with more than one output are important for synthesis and design approaches in the current-mode (CM) [1]. There exists commercially available devices like diamond transistor [2], transconductance amplifier [3], current conveyor or current feedback amplifier [4], etc. but they usually do not have more than one output. Many devices and structures in the current-mode require multi-output active elements that have not been commercially available yet. This improvement enables to use of commercially available active elements in CM. This element is also very important for many applications i.e. current or mixed mode multi-loop integrator synthesis of active filters, harmonic or nonlinear oscillators, amplifiers, current-mode operations (distribution and mirroring), etc.

2. CURRENT FOLLOWER WITH TWO OUTPUTS

The schematic symbol of current follower based on simple current mirrors [5, 6] with two positive current outputs is in Fig. 1(a) and his structure in Fig. 1(b). Circuit in Fig. 1(b) was built from discrete transistors type BC547A and BC557A [7]. Easy but more complicated modification for both polarities is in Fig. 2. However, there are additional transistors.

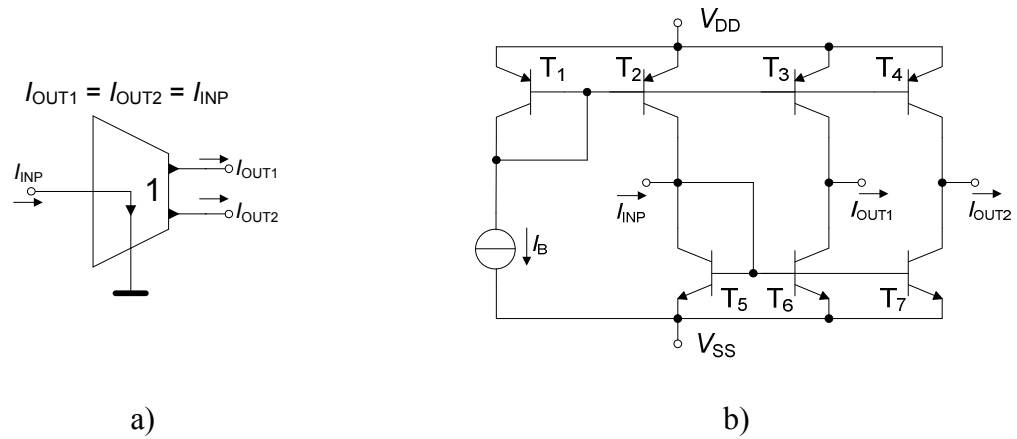


Figure 1: a) Symbol of current follower with two positive outputs, b) transistor implementation

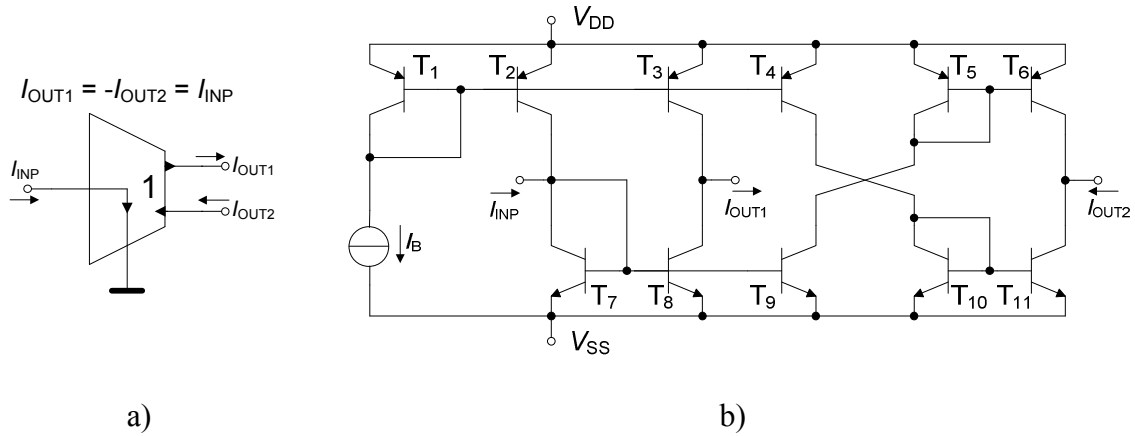


Figure 2: a) Symbol of current follower with positive and negative output, b) transistor implementation

3. ANALYSIS AND MEASUREMENT RESULTS

For measurement (see Fig. 3) was necessary input converter with diamond transistor OPA 660 [2] and output loads with voltage buffers BUF 634 [8] for impedance separation. Bias current I_B was set 1000 μA .

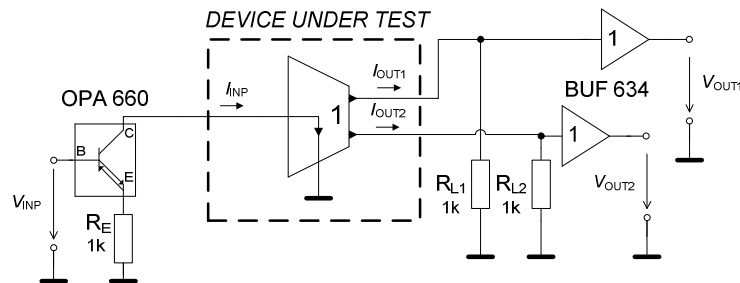


Figure 3: Analyzed and measured testing circuit

The voltage to current and current to voltage conversion we can describe by following fundamental expressions

$$g_m \approx 1/R_E, I_{INP} = g_m V_{INP}, V_{OUT1} = R_{L1} I_{OUT1}, V_{OUT2} = R_{L2} I_{OUT2}. (1), (2), (3), (4)$$

The CF (see Fig. 1) was tested in the frequency domain. Results of simulation in PSpice are in Fig. 4 and results of measurement are in Fig. 5. Network analyzer Agilent E5071C was used for experimental tests in frequency domain. Simulation result show that -3 dB drop is about 7.6 MHz. From measurement results is obvious that -3 dB drop is only 2 – 3 MHz. The CF circuit was measured at solderless field and there are many influences mainly on higher frequencies (quite high parasitic capacitances). Simulated and measured input-output characteristics are depicted in Fig. 6. Important small signal parameters dependent on frequency like Z_{INP} and Z_{OUT} are in Fig. 7. Accordingly to Fig. 7 is clear that change of I_B effects these parameters. In some cases [9] adjusting of R_{INP} is required for electronic adjusting of some parameters (in filters, oscillators). It is suitable only in finite range because output impedance is also I_B and frequency depending and this effect has negative impact for example on attenuation in stop-bands of active filters [10].

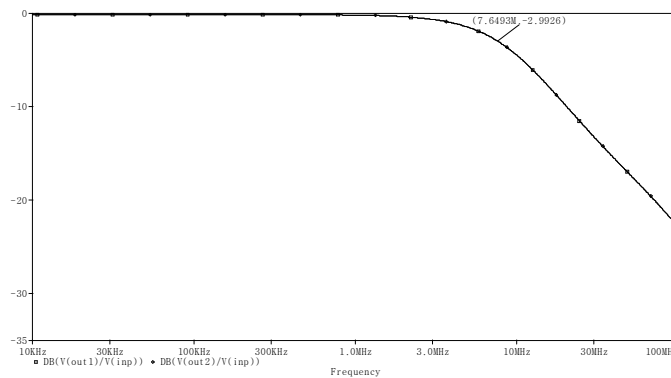
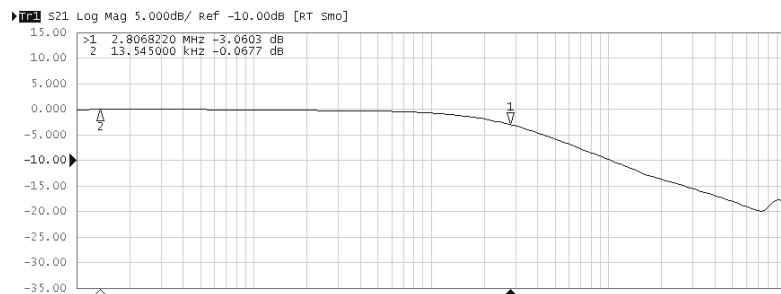
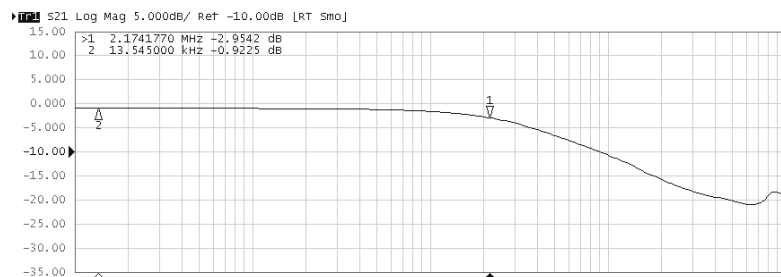


Figure 4: Magnitude responses of current follower



a)



b)

Figure 5: Measured magnitude responses (range 10 kHz – 100 MHz) a) OUT_1 , b) OUT_2

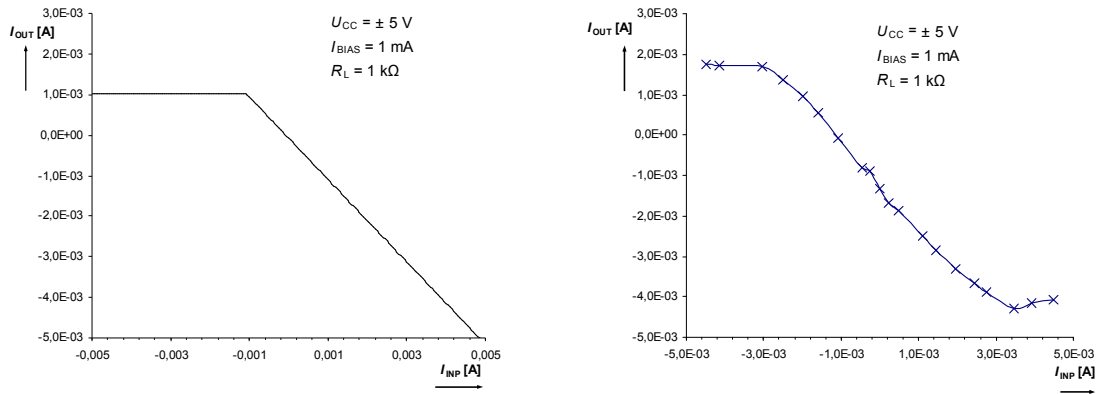


Figure 6: a) Simulated and b) measured input-output characteristics

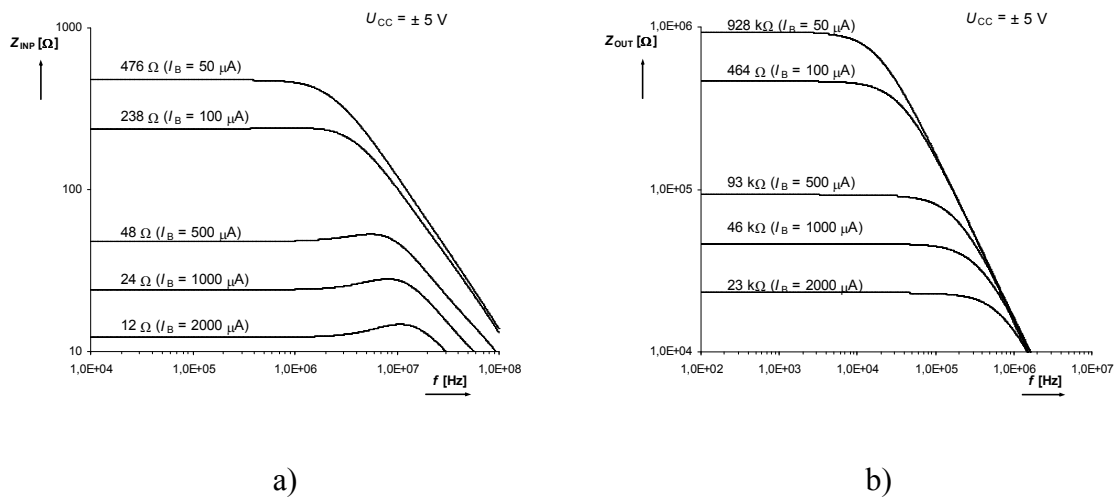


Figure 7: Dependence of a) input impedance, b) output impedance on frequency for different bias current values (simulations)

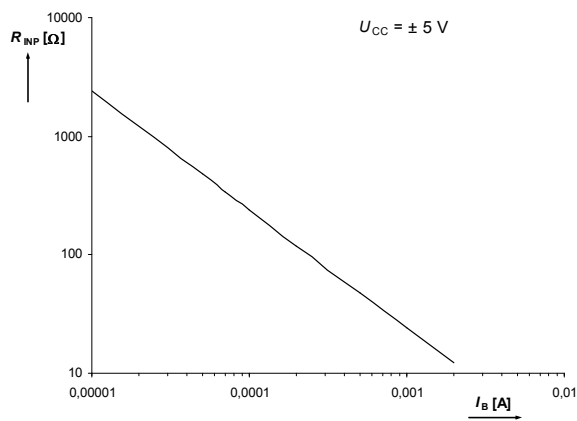


Figure 8: Dependence of R_{INP} on I_B

4. CONCLUSION

Presented way how to realize current follower with more than one output was practically verified. More or less simulation and measurement results confirmed theory presumptions but there were many influences on frequency response and input offset. However, functionality of presented circuit was verified and in some unpretentious cases can be sufficient. Circuit has quite good dynamical range of several mA in comparison with low power CMOS structures where it is about maximally several hundreds of μA . Frequency response is not much satisfactory. Next part of work will be focused on realizations based on commercially available integrated transistor fields HFA 3127/3128 [11] where we can expect better results first of all in frequency domain.

ACKNOWLEDGEMENT

Research described in the paper was supported by the Czech Ministry of Education under research program MSM 0021630513 and Czech Science Foundation projects under No. 102/08/H027, No. 102/09/1681 and 102/09/P217. Research described in the paper is a part of the COST Action IC0803 RF/Microwave communication subsystems for emerging wireless technologies, financed by the Czech Ministry of Education by the grant no. OC09016.

REFERENCES

- [1] TOUMAZOU, C., LIDGEY, F. J., HAIGH, D. G. Analogue IC design: The current mode approach, Peter Peregrinus Ltd., London, 1990
- [2] Texas Instruments Inc. OPA 660/860 Wide Bandwidth Operational Transconductance Amplifier and Buffer. 2006, 32 p. accessible on www: <http://www.ti.com>
- [3] Linear Technology. LT 1228 - 100 MHz current-feedback amplifier with DC gain control. 1994, 20 p., accessible on www: <http://www.linear.com>
- [4] Analog Devices. Monolithic Op Amp AD 844, 16 p., available on www: <http://www.analog.com>
- [5] SOULIOTIS, G., HARITANTIS, I. Current-mode filters based on current mirror arrays. *Int. Journal of Circuit Theory and Applications*, 2008, vol. 36, pp. 173-183.
- [6] SOULIOTIS, G., PSYCHALINOS, C. Current-Mode Linear Transformation Filters Using Current Mirrors. *IEEE Transaction on Circuits and Systems-II: Express Briefs*, 2008, vol. 55, no. 5, pp. 541-545.
- [7] ON Semiconductor, BC547/BC557 NPN/PNP Amplifier Transistor Silicon Plastic. 2007, 6 p., accessible on www: <http://www.onsemi.com/>
- [8] Texas Instruments. BUF 634 250 mA High speed buffer. 2000, 14 p., accessible on www: <http://www.ti.com>
- [9] SIRIPRUCHYANUN, M., CHANAPROMMA, C., SILAPAN, P., JAIKLA, W. BiCMOS Current-Controlled Current Feedback Amplifier (CC-CFA) and Its Applications. *WSEAS Transactions on Electronics*, 2008, no. 6, vol. 5, pp. 203-219.
- [10] SOTNER, R., PETRZELA, J., SLEZAK, J. Current-Controlled Current-Mode Universal Biquad Employing Multi-Output Transconductors. *Radioengineering*, 2009, vol. 18, no. 3, pp. 285-294.
- [11] Data sheet HFA 3046/3096/3127/3128, Transistor Array SPICE Models, Application Note 1994, accessible on www: <http://www.intersil.com>.